



Motivation

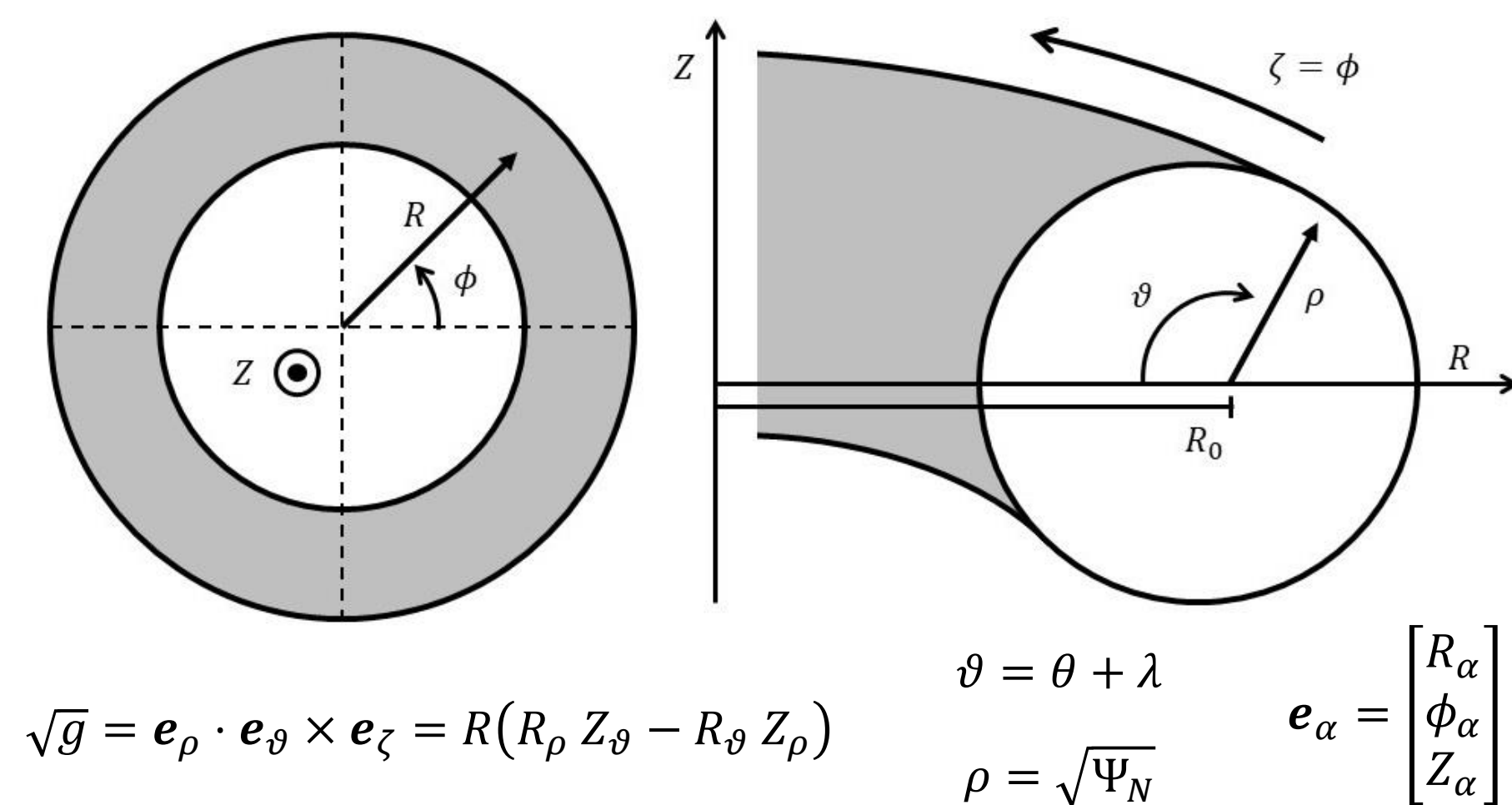
Accurate and efficient equilibria calculations in fusion devices are crucial for understanding plasma science, improve diagnostics, avoiding disruptions, and enabling control systems. Conventional equilibria codes for non-axisymmetric geometries are computationally expensive and can return results that are poor solutions to the equilibrium force balance. We have developed a new code that directly solves the force balance equations and has the potential to converge faster than energy minimization approaches. As modern stellarator experiments continue to show a promising path to fusion, the development of advanced three-dimensional equilibria codes is becoming increasingly important.

Ideal MHD Equilibrium

Under the ideal MHD model of plasmas, the equilibrium condition reduces to a momentum balance, Ampere's Law, and the absence of magnetic monopoles [1]:

$$\mathbf{J} \times \mathbf{B} = \nabla p \quad \nabla \times \mathbf{B} = \mu_0 \mathbf{J} \quad \nabla \cdot \mathbf{B} = 0$$

An equilibrium is typically constructed by prescribing the pressure profile $p(\rho)$ then numerically solving for the magnetic field \mathbf{B} that satisfies the equilibrium conditions. The following diagram shows the toroidal (R, ϕ, Z) and straight field line (ρ, ϑ, ζ) coordinate systems [2]:



$$\sqrt{g} = \mathbf{e}_\rho \cdot \mathbf{e}_\vartheta \times \mathbf{e}_\zeta = R(R_\rho Z_\vartheta - R_\vartheta Z_\rho)$$

$$\vartheta = \theta + \lambda$$

$$\rho = \sqrt{\Psi_N}$$

$$\mathbf{e}_\alpha = \begin{bmatrix} R_\alpha \\ \phi_\alpha \\ Z_\alpha \end{bmatrix}$$

Conventional Approach

The existence of flux surfaces and the rotational transform profile provide two additional constraints on the equilibrium problem:

$$\mathbf{B} \cdot \nabla p = 0 \quad \iota = \frac{B^\vartheta}{B^\zeta}$$

Most equilibria construction codes, including VMEC, solve for an equilibrium by minimizing the total energy of the plasma [3]:

$$W = \int \left(\frac{|\mathbf{B}|^2}{2\mu_0} + p \right) dV$$

Poincaré Sections Approach

Instead of minimizing the total energy, the equilibrium force balance is used as a constraint to derive a system of ordinary differential equations that describe the "flow" of flux surfaces around the torus. The force balance can be written in the form [3]

$$(\nabla \times \mathbf{B}) \times \mathbf{B} - \mu_0 \nabla p = \mathbf{0}$$

$$\mathbf{F} \equiv F_\rho \nabla \rho + F_\beta \boldsymbol{\beta} = \mathbf{0}$$

$$F_\rho = \frac{1}{\mu_0} (B^\vartheta (\partial_\rho B_\vartheta - \partial_\vartheta B_\rho) + B^\zeta (\partial_\rho B_\zeta - \partial_\zeta B_\rho)) + p'$$

$$F_\beta = \frac{1}{\mu_0 \sqrt{g}} (\partial_\vartheta B_\zeta - \partial_\zeta B_\vartheta) \quad \boldsymbol{\beta} = \sqrt{g} (B^\zeta \nabla \vartheta - B^\vartheta \nabla \zeta)$$

Since $\nabla \rho$ and $\boldsymbol{\beta}$ are independent directions, the condition $F_\rho = F_\beta = 0$ must hold in equilibrium. This yields two additional equations:

$$F_\rho = 0 \Rightarrow \partial_\zeta B_\rho = \iota (\partial_\rho B_\vartheta - \partial_\vartheta B_\rho) + \partial_\rho B_\zeta + \mu_0 \frac{p'}{B^\zeta}$$

$$F_\beta = 0 \Rightarrow \partial_\zeta B_\vartheta = \partial_\vartheta B_\zeta$$

Satisfying the divergence-free field and assuming nested flux surfaces, the magnetic field can be written in the contravariant form

$$\mathbf{B} = B^\vartheta \mathbf{e}_\vartheta + B^\zeta \mathbf{e}_\zeta = B^\zeta (\iota \mathbf{e}_\vartheta + \mathbf{e}_\zeta) \quad B^\zeta = \frac{\Psi'}{2\pi \sqrt{g}}$$

Substituting this form of the magnetic field into the two equilibrium conditions above yields equations for $\dot{R}(\rho, \vartheta, \zeta)$ and $\dot{Z}(\rho, \vartheta, \zeta)$. This formulation allows the task of solving for an equilibrium to be converted into a boundary-value problem (BVP) with a system of ordinary differential equations and periodic boundary condition:

$$\mathbf{x}(\zeta) = \begin{bmatrix} R(\rho, \vartheta) \\ Z(\rho, \vartheta) \\ \lambda(\rho=1) \\ \dot{R}(\rho, \vartheta) \\ \dot{Z}(\rho, \vartheta) \\ \dot{\lambda}(\rho=1) \end{bmatrix} \quad \dot{\mathbf{x}} = \begin{bmatrix} \dot{R} \\ \dot{Z} \\ \dot{\lambda} \\ \frac{2\pi R}{\Psi'} (k_\rho Z_\vartheta - k_\beta Z_\rho) \\ -\frac{2\pi R}{\Psi'} (k_\rho R_\vartheta - k_\beta R_\rho) \\ \frac{\mathbf{e}_\vartheta \cdot (\mathbf{e}_{\theta\theta} \dot{\theta}^2 + 2 \mathbf{e}_{\theta\phi} \dot{\theta} + \mathbf{e}_{\phi\phi}) - \frac{k_\beta}{B^\zeta}}{\mathbf{e}_\vartheta \cdot \mathbf{e}_\theta} \end{bmatrix} = f(\zeta, \mathbf{x})$$

$$\mathbf{x}(0) = \mathbf{x}(2\pi)$$

$$k_\rho = \iota (\partial_\rho B_\vartheta - \partial_\vartheta B_\rho) + \partial_\rho B_\zeta + \mu_0 \frac{p'}{B^\zeta}$$

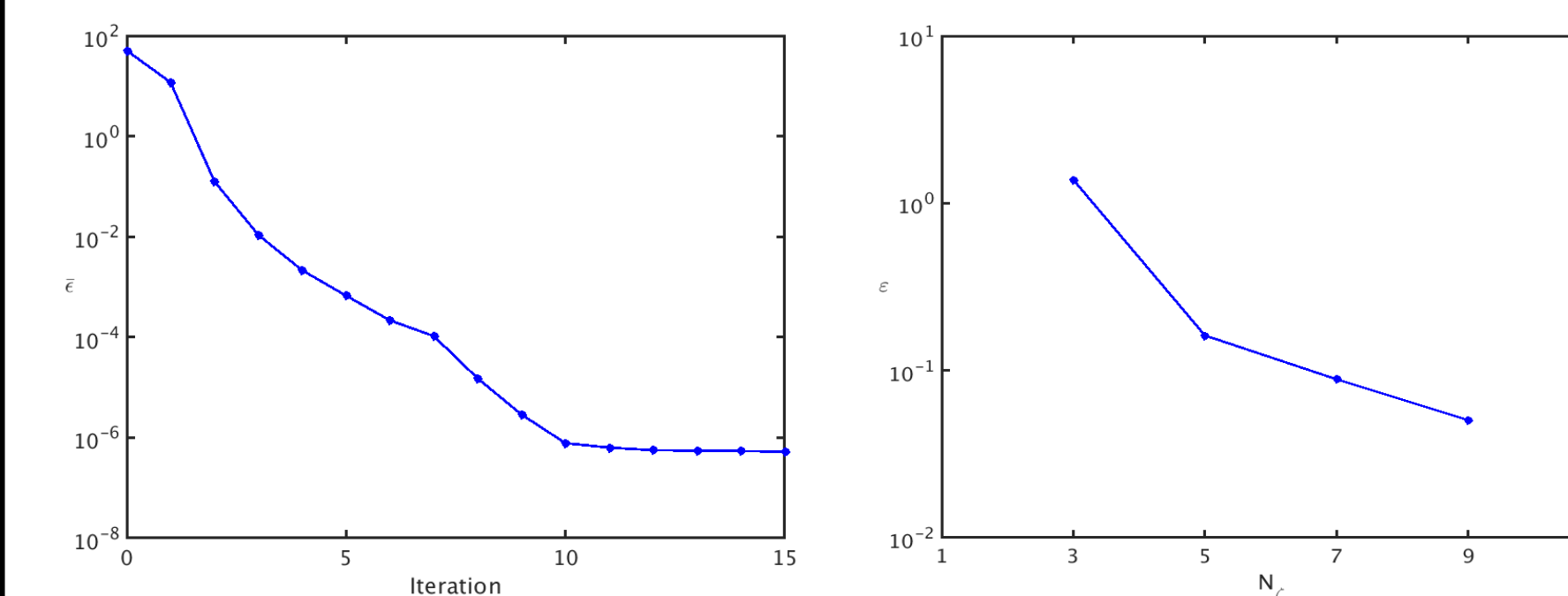
$$-\partial_\zeta B^\zeta (\iota \mathbf{e}_\rho \cdot \mathbf{e}_\vartheta + \mathbf{e}_\rho \cdot \mathbf{e}_\zeta) - B^\zeta (\mathbf{e}_{\rho\zeta} \cdot (\iota \mathbf{e}_\vartheta + \mathbf{e}_\zeta) + \iota \mathbf{e}_\rho \cdot \mathbf{e}_{\vartheta\zeta})$$

$$k_\beta = \partial_\vartheta B_\zeta - \partial_\zeta B^\zeta (\iota |\mathbf{e}_\vartheta|^2 + (\mathbf{e}_\vartheta \cdot \mathbf{e}_\zeta)) - B^\zeta \mathbf{e}_{\vartheta\zeta} \cdot (2\iota \mathbf{e}_\vartheta + \mathbf{e}_\zeta)$$

The variable λ is used instead of R and Z at the last closed flux surface where the fixed-boundary $R(\theta), Z(\theta)$ is given as a constraint. The unknowns \mathbf{x} are defined on a Poincaré section at a given toroidal angle ζ . The periodic boundary condition arises since the equilibrium Poincaré section must represent the same flux surfaces after integrating over a full field period.

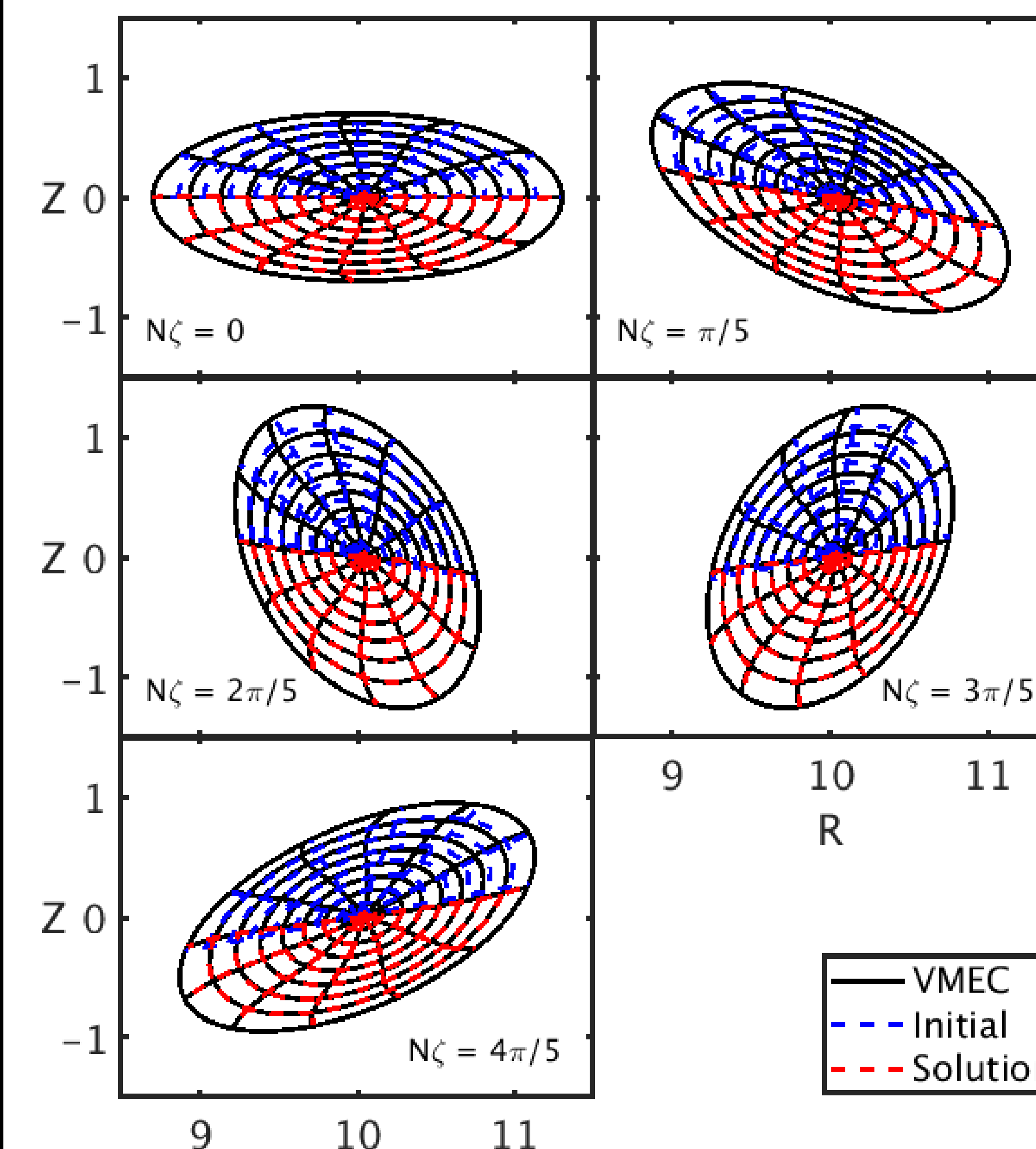
Comparison to VMEC

The computational polar domain is discretized using pseudo-spectral methods with a Fourier series in ϑ and Chebyshev polynomials in ρ [4]. The BVP is solved using a spectral collocation approach with a Fourier series expansion in ζ .



Left: Normalized sum of squares of the residuals at each iteration of the Levenberg-Marquardt algorithm used to solve the BVP.

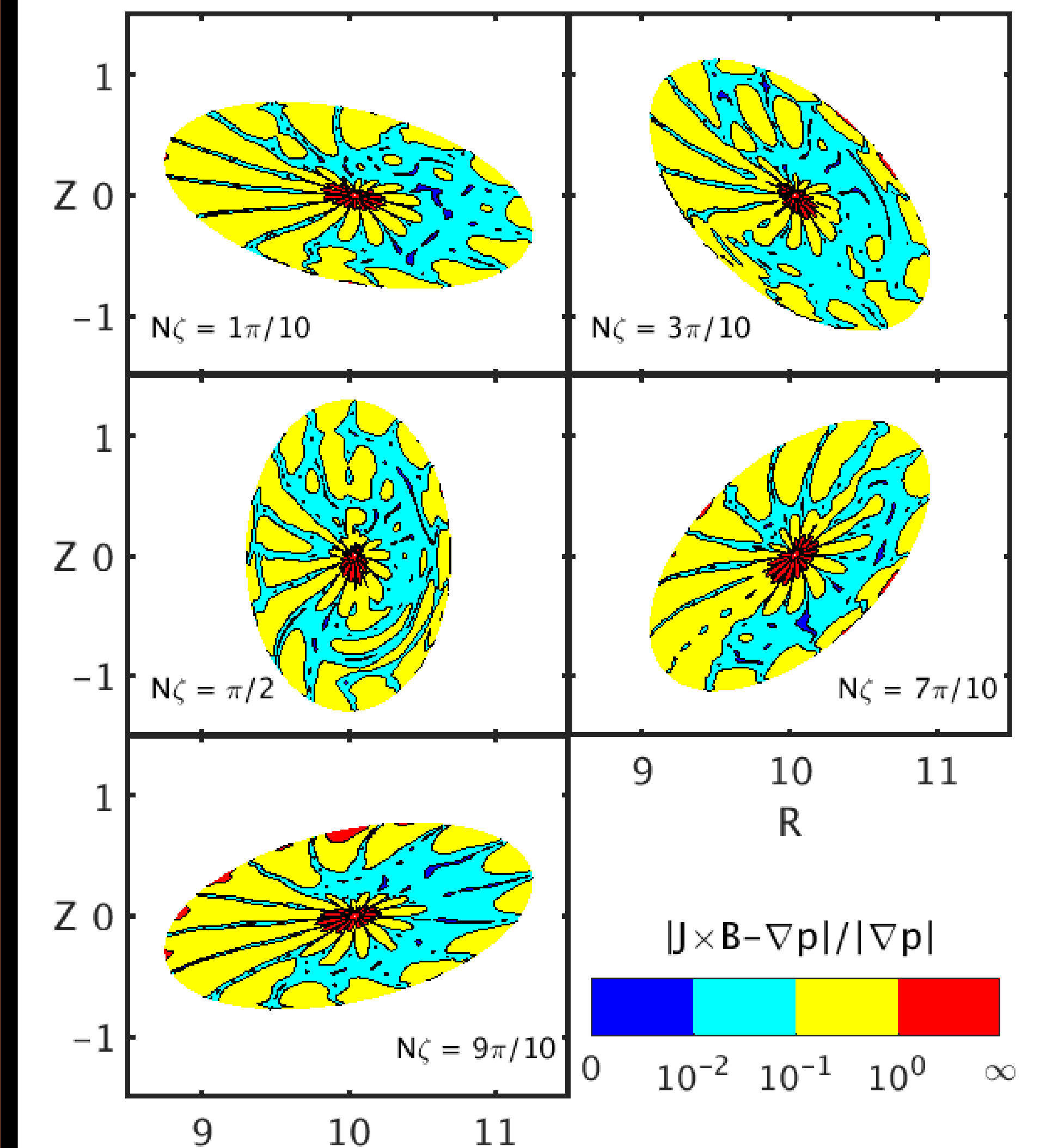
Right: $|\mathbf{x}(0) - \mathbf{x}^{VMEC}(0)|$ as a function of the number of Fourier modes used in the toroidal expansion (number of Poincaré sections).



Above: Comparison of flux surfaces between the BVP solution and VMEC equilibrium. The initial guess for the solution was obtained by scaling the boundary surface proportional to ρ .

Error Quantification

Below: Equilibrium force balance error $|\mathbf{F}|/|\nabla p|$ for the BVP solution. The system of equations $\dot{\mathbf{x}} = f(\zeta, \mathbf{x})$ is equivalent to the equilibrium constraints, so the approach directly minimizes the error at the collocation points. The midpoints of the toroidal angles where $\mathbf{x}(\zeta)$ is defined are shown.



All the results presented are for a heliotron with the following boundary and profile inputs:

$$R = 10 - \cos \theta - 0.3 \cos(\theta - N\phi) \quad Z = \sin \theta - 0.3 \sin(\theta - N\phi)$$

$$p(\rho) = p_0(1 - \rho^2) \quad \iota(\rho) = 1.618$$

with the number of field periods $N = 19$ and p_0 corresponds to $\beta = 1.1\%$. A basis of 8 Fourier modes and 8 Chebyshev polynomials were used.

Future Work

- Refine numerical methods to improve accuracy and convergence rate
- Develop tools to investigate stability of equilibria and the existence of neighboring solutions (see other poster)
- Restructure the boundary condition for free-boundary equilibria
- Formulate a method to allow for magnetic islands and chaotic regions